## SAAB JA-37 Viggen

## Performance Assessment

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## SAAB JA-37 Viggen Performance Assessment

## 1. Overview

 is Swedish for "Thunderbolt". The aircraft has been built in several versions, as follows;

```
AJ-37 single seat all weather attack
JA-37 single seat air defence
SF-37 single seat armed photo reconnaissance
SH-37 single seat armed sea surveillance
SK-37 dual seat conversion trainer
```


 production JA-37 on the 4th of November 1977.
 this information to produce a performance estimate for the aircraft.

## 2. Dimensions

 and weights are provided in metric units, then converted to imperial units.

| Wing Span | 10.60 metres | 34 feet 9.25 inches |
| :--- | :--- | :--- |
| Foreplane Span | 5.45 metres | 17 feet 10.5 inches |
| Main Wing Aspect Ratio 2.45 |  |  |


| Length <br> Length | 15.45 metres | 50 feet 8.25 inches |
| :--- | :--- | :--- |
| Length | 16.30 metres | 53 feet 5.75 inches | | (AJ, excluding probe) |
| :--- |
| Length |
| (AJ, including probe) |
| Height |
| Height |


| Total Lifting Area | 52.20 square metres | $561.88 \mathrm{sq.ft}$ | (including foreplanes) |
| :--- | ---: | ---: | :--- |
| Gross Wing Area | 46.00 square metres | $495.16 \mathrm{sq.ft}$ | (wing alone) |
| Foreplane Area | 6.20 square metres | $66.74 \mathrm{sq.ft}$ | (nett) |

Note: the gross wing area is the area of the main wing, including that portion which carries across the fuselage. The foreplane area is the area of the lifting surfaces, not including the portion which carries through the fuselage. The "total wing area" defined in some areas is the sum of the gross wing area and nett foreplane area, and can be misleading.

## 3. Weights

Only limited weight data (in metric units) has been provided for the aircraft. The following is my best estimate for the actual weights of the aircraft and its component parts.

| Empty Weight | $12,200 \mathrm{~kg}$ | $26,895 \mathrm{lbs}$ | (approx) |
| :--- | :--- | :--- | :--- |
| Normal Loaded | $16,800 \mathrm{~kg}$ | $37,040 \mathrm{lbs}$ | (carrying four AAM) |
| Max Takeoff | $22,500 \mathrm{~kg}$ | $49,600 \mathrm{lbs}$ |  |

Up to $6,000 \mathrm{~kg}(13,227 \mathrm{lbs})$ of ordnance can be carried externally.

| Takeoff weight | $15,000 \mathrm{~kg}$ | $33,070 \mathrm{lbs}$ | (clean) |
| :--- | :--- | :--- | :--- |
| Takeoff weight | $17,000 \mathrm{~kg}$ | $37,478 \mathrm{lbs}$ | (normal armament) |

The cannon has 150 rounds, at 0.36 kg ( 0.79 lbs ) per round for a total weight of 54 kg .


## Weight Breakdown

Assuming the figure of $12,200 \mathrm{~kg}$ for a clean, empty aircraft is approximately correct, we can now check one of the other weights to see if it corresponds. An empty aircraft is the condition of the aircraft being fully equipped but with no fuel, pilot or external stores. We have a value for a normal loaded aircraft, which gives us a weight of $17,000 \mathrm{~kg}$ when fitted with 4 air-to-air missiles. If we add weights for a pilot and full internal fuel, plus four Rb-24 missiles (AIM-9L), we get the following;

| Clean A/C | $12,200 \mathrm{~kg}$ | (includes 150 rounds for gun) |
| :--- | ---: | :--- |
| Pilot | 100 kg |  |
| Fuel (100\% internal) | 4440 kg | (at $6.5 \mathrm{lbs} / \mathrm{US}$ gallon) |
| $4 \times$ Aim-9L | 342 kg |  |
| Total | ..------- |  |

This corresponds approximately to the weight expected. So we can now propose a weight breakdown for the aircraft and its component parts.

| Clean A/C | $12,200 \mathrm{~kg}$ | $(54 \mathrm{~kg}$ for 150 rounds for gun) <br> $(600 \mathrm{~kg}$ for avionics) |
| :--- | ---: | :--- |
| Pilot |  |  |
| Fuel (100\% internal) | 100 kg |  |
| Rb-24 (AIM-9L) | 4440 kg for engine) |  |

## 4. Ordnance

The aircraft is typically configured to have up to seven (7) external pylons. These are located as follows (with estimated load limits at each location);

| $1 \times$ centreline pylon | 2000 kg | 4410 lbs |
| :--- | ---: | ---: |
| $2 \times$ fuselage edge pylons | 500 kg | 1102 lbs |
| $2 \times$ inner wing pylons | 1000 kg | 2205 lbs |
| $2 \times$ outer wing pylons | 500 kg | 1102 lbs |

A typical air defence loading would include $2 \times \mathrm{Rb} 72$ Skyflash and 2 or $4 \times \mathrm{Rb} 24$ Sidewinder (AIM-9L) missiles. The aircraft is fitted with a single 30 mm Oerlikon KCA cannon. This has 150 rounds available.

## 5. Engine

The aircraft is fitted with a Volvo Flygmotor RM-8 turbofan engine. This is based on the Pratt \& Whitney JT-8D-22 engine, with a Volvo designed afterburner fitted. The engine has two versions. The RM-8A is fitted to all except the JA version of the aircraft. The JA is fitted with the RM-8B engine; a slightly more powerful version of the engine.

## Thrust

| RM-8A | 25, 970 lbst | 11790 kg | max reheat |
| :--- | :--- | ---: | :--- |
|  | 14,750 lbst | 6690 kg | max dry |
| RM-8B | 28,110 lbst | 12750 kg | max reheat |
|  | 16,200 lbst | 7350 kg | $\max$ dry |

Fuel Consumption

| RM-8A | $2.47 \mathrm{lb} / \mathrm{hr} / \mathrm{lbst}$ | $70.0 \mathrm{mg} / \mathrm{Ns}$ | $\max$ reheat |
| :--- | :--- | :--- | :--- |
|  | $0.63 \mathrm{lb} / \mathrm{hr} / \mathrm{lbst}$ | $17.8 \mathrm{mg} / \mathrm{Ns}$ | $\operatorname{max~dry}$ |
|  | $0.61 \mathrm{lb} / \mathrm{hr} / \mathrm{lbst}$ | $17.3 \mathrm{mg} / \mathrm{Ns}$ | $\max$ continuous |
|  |  |  |  |
| RM-8B | $2.52 \mathrm{lb} / \mathrm{hr} / \mathrm{lbst}$ | $71.4 \mathrm{mg} / \mathrm{Ns}$ | $\max$ reheat |
|  | $0.64 \mathrm{lb} / \mathrm{hr} / \mathrm{lbst}$ | $18.1 \mathrm{mg} / \mathrm{Ns}$ | $\max$ dry |
|  | $0.61 \mathrm{lb} / \mathrm{hr} / l \mathrm{bst}$ | $17.3 \mathrm{mg} / \mathrm{Ns}$ | $\max$ continuous |

## Dimensions

| Length | 6.17 metres | RM-8A |
| :--- | :--- | :--- |
|  | 6.24 metres | RM-8B |
| Max Diameter | 1.397 metres | 55 inches |
| Inlet Diameter | 1.030 metres | 40.55 inches |
| Max Mass Flowrate | $145 \mathrm{~kg} / \mathrm{sec}$ |  |
| Bypass Ratio | 1.10 |  |
| Max Pressure Ratio | 16.5 |  |

## Pratt \& Whitney JT-8D-7 Turbofan

For comparison purposes the key performance data for the JT-8 engine are provided here. This is a non-afterburning engine.

| 6350 kg nett thrust - takeoff - sea level static |  |
| :--- | :--- |
| 1540 kg nett thrust - cruise - Mach 0.80 at 11,000 metres |  |
|  |  |
| Cruise sfc | $0.81 \mathrm{~kg} / \mathrm{kg} / \mathrm{hour}$ |
| Bypass Ratio | 1.10 |
| Air Flow | $141 \mathrm{~kg} / \mathrm{sec}$ at sea level static conditions |
| Pressure Ratio | 15.8 |
| Internal Diameter | 0.108 metres |
| Length | 3.75 metres |
| Dry Weight | 1431 kg |
| No of Spools | 2 |

## 6. Performance

The following performance and mission profile data is the best estimate from the various sources of data found.

| Max Speed at Seal Level $(4 \times$ AAM $)$ | 838 mph | 1350 kmh | Mach 1.10 |
| :--- | :--- | :--- | :--- | :--- |
| Max Speed at 11, 000 metres | 1365 mph | 2195 kmh | Mach 2.1 |$\quad$ (at 36,090 ft)

## Mission Profiles

Ferry range 2000 km (2250 km with Jet-A fuel)
Tactical Radius

| - intercept mission | 250 miles $\quad 400 \mathrm{~km}$ |
| :--- | :--- |
| - hi-lo-hi profile | 621 miles (with unspecified external stores) |
| - lo-lo-lo profile 311 miles (with unspecified external stores) |  |

For external load of $4 \times 1000 \mathrm{lbs}(454 \mathrm{~kg})$ bombs and fuel
Tactical Radius

$$
\begin{aligned}
& \text { - hi-lo-hi profile } \quad 782 \text { miles } \\
& \text { - lo-lo-lo profile } 532 \text { miles }
\end{aligned}
$$

## 7. Take-0ff

The aircraft was initially designed to operate from narrow 500 m long runways (1640 feet). Tha actual take-off run is approximately 400 metres ( 1310 feet). The key points in the aircraft take-off are as follows;

Afterburner is selected then the wheel brakes are released.
The aircraft accelerates to a rotation speed of 135 knots (250 kmh).
About 600 metres of runway is used to get airborne.
After lift-off the undercarriage is retracted and the aircraft accelerates at a 2 to 3 degree climb angle to 367 knots ( 680 kmh ).

Below 190 knots ( 350 kmh ) the aircraft is very sensitive in roll.
Afterburner is cut out at 270 knots ( 500 kmh ) due primarily to noise abatement requirements.
Exceeding 30 degrees angle of attack results in some loss of yaw stability.
Over 30 degrees AOA the aircraft will enter into a "super stall", but is easily recoverable.
There is little natural pre-stall warning, with low buffet levels.

## 8. Landing

| Landing Run | approx 500 m |
| :--- | :--- |
| Landing Speed | 220 kmh |

The undercarriage is lowered.
The thrust reverser is pre-selected to activate immediately after landing.
The approach is steep.
The aircraft attitude is 15 degrees nose up.
The speed is controlled by the autopilot.
The aircraft crosses the runway threshold at 130 knots (240 kmh).
Touchdown with a no-flare landing at 97 knots (180 kmh).
Touchdown is about 45 metres (150 feet) beyond the runway threshold.
The undercarriage is designed for a landing sink rate of 16 feet/sec (5 m/s).

## 9. References

Jane's All the World's Aircraft 1985-86
Modern Combat Aircraft Design
by Klaus Huenecke
Airlife Publishing Ltd 1987
The Illustrated Encyclopedia of the World's Modern Military Aircraft
by Bill Gunston
Salamander Books Ltd 1977
The New Observer's Book of Aircraft
by William Green
Frederick Warne \& Co 1986
Modern Air Combat
by Bill Gunston and Mike Spick Salamander Books Ltd 1983

Attack Aircraft
by Roy Braybrook Haynes Publishing Group 1990

World Aircraft Information File - Issue 47
Aerospace Publishing Ltd 1998
Air International - Volume 56 No 2
Key Publishing Ltd February 1999
Aeronautical Vest Pocket Handbook
Pratt \& Whitney June 1978

## 10. Conversion Factors

The following conversion factors between metric and Imperial units were used at various places in this document.

| 3.281 feet | $=1.0$ metre |
| :--- | :--- |
| 10.76 square feet | $=1.0$ square metres |
| 2.205 pounds | $=1.0$ kilogram |
| 3.785 litres | $=1.0$ US gallon |
| 4.545 litres | $=1.0$ Imperial Gallon |
| 1 knot | $=6080$ feet per second |
| 1 mile per hour | $=5280$ feet per second |
| 1.097 feet per second | $=1.0$ kilometre per hour |

11. Liquid Weights

The following liquid densities were used to determine the fuel weights for the aircraft.

| JP-1 | $6.65 \mathrm{lbs} /$ US gal |
| :--- | :--- |
| JP-3 | $6.45 \mathrm{lbs} /$ US gal |
| JP-4 | $6.55 \mathrm{lbs} /$ US gal |
| JP-5 | $6.82 \mathrm{lbs} /$ US gal |
| Jet-A | $6.74 \mathrm{lbs} /$ US gal |
| Gasoline | $5.87 \mathrm{lbs} / \mathrm{US}$ gal |
| Water | $8.345 \mathrm{lbs} /$ US gal |

## Appendix A: Calculated Aircraft Dimensions

The following dimensions and areas have been determined by scanning a 3-view drawing of the Viggen, then importing it into a CAD program, scaling it appropriately and measuring the specific values shown here. Many of these values will be required for a theoretical drag estimation of the aircraft and other aspects of the performance assessment.

No specific wing section data has been found so the values shown are estimates only, based on standard design assumptions.

Wing
Approximately $4 \%$ thick, with maximum thickness at $40 \%$ of chord.

| Root Chord 24.9 feet | Tip Chord | 1.8 feet | Taper Ratio 0.07 |
| :--- | :--- | :--- | :--- | :--- |
|  |  |  |  |
| Sweep of Quarter Chord Line | 42 degrees |  |  |
| Wing Semi-Span | 17.5 feet |  |  |
| Wing Span | 35.0 feet |  |  |
| Gross Wing Area | 522 square feet |  |  |

## Foreplane

Approximately 6\% thick, with maximum thickness at 40\% of chord.

| Root Chord 1.0 feet | Tip Chord | Taper Ratio 0.2 feet |  |
| :--- | :--- | :--- | :--- |
| Sweep of Quarter Chord Line | 50 degrees |  |  |
| Panel Span | 5.3 feet |  |  |
| Panel Area | 35.0 square feet |  |  |
| Geometric Aspect Ratio | 0.80 |  |  |

## Vertical Fin

Approximately $5 \%$ thick, with maximum thickness at $40 \%$ of chord.
Root Chord
13.6 feet
Tip Chord
1.6 feet
Taper Ratio
0.12
Sweep of Quarter Chord Line
Span
Area
Geometric Aspect Ratio
43 degrees
9.0 feet
68.7 square feet
1.20

Fuselage
Length 50.0 feet $\quad$ Width 8.25 feet 7.0 feet

Frontal Area 42 square feet
Surface Area 880 square feet

## Appendix B: Calculated Aerodynamic Data

## Calculation of Maximum Lift Coefficient

It is possible to make an estimate of the maximum lift coefficient for the aircraft. Available data states the aircraft approach speed is 119 knots, which will be a speed just above the stall speed of the aircraft.

Assuming 119 knots is the aircraft stall speed, we know the wing area and air density, and can approximate the aircraft weight, and so find the lift coefficient for this condition.

We will assume the atmospheric conditions are for sea level and standard ISA conditions. This gives an air mass density of 0.002378 slugs per cubic foot. Also, 119 knots is equal to 201 feet per second.

We have a gross wing area of 562 square feet. Because the aircraft is of canard configuration, the foreplanes generate lift as well as the main wing, so both contribute to the total aircraft lift.

We will assume a standard weight condition for the aircraft for all subsequent analysis. Much of the tactical radius data obtained is for an aircraft in an air defence configuration, carrying 4 air to air missiles. We will assume this is for two short range ((AIM-9L) and two long range (SkyFlash) missiles. It is also normal practice to assume a $50 \%$ fuel load for performance analysis such as this, so we will assume a $50 \%$ internal fuel load and no external fuel.

This then gives a weight of 33,244 pounds (15,077 kilograms).

| Clean A/C | $12,200 \mathrm{~kg}$ |
| :--- | ---: |
| Pilot | 100 kg |
| Fuel (50\% internal) | 2220 kg |
| $2 \times$ SkyFlash | 386 kg |
| $2 \times$ Aim-9L | 171 kg |
| Total | $---.-15,077 \mathrm{~kg}$ |

33,244 pounds

```
CL = (2 x Weight) / (rho x area x velocity x velocity)
CL = (2 x 33,244) / (0.002378 x 562 x 201 x 201)
CL = 1.23
```

In practice the actual lift coefficient will be probably be somewhere between 1.25 and 1.30 but a value of 1.23 (based on a reference wing area of 562 square feet) is a safe value for controlled flight at a minimum speed.

## Appendix C: Performance Analysis

Based on the data presented here, a performance estimate for the Viggen has been prepared. This was generated using the suite of computer programs produced by Mr Sidney A Powers, called "BASIC Aircraft Performance" (Kern International, Inc. Copyright 1984).

This suit of programs includes routines to predict aircraft drag, format engine data and determine various aircraft performance parameters, including mission analysis and flight performance at varying altitudes.

## DRAG ESTIMATE

These routines were used to iteratively obtain a likely drag for the Viggen aircraft, then to determine other data, including flight envelopes at various load factors, turning performance and mission performance for varying stores configurations.

In obtaining a drag estimate for the aircraft it is always necessary to define this in relation to the aircraft's engine performance. The engine performance (thrust and fuel flow, and their variation with speed and altitude) was estimated based on the best data available, but cannot be guaranteed to truly represent the Viggen engine. So the drag data presented is that which corresponds to the engine data used here. If another engine computer model is used to generate engine performance then the drag values may need to be adjusted to suit.

Drag is presented in the typical way for computer analysis, as a profile drag coefficient and a wing spanwise efficiency factor. Together these will define the drag polar for the aircraft. These values have been provided at a range of aircraft speeds, to allow for the relative effects of subsonic, transonic and supersonic flow. That is,

| CDo | = | Profile Drag Coefficient |
| :---: | :---: | :---: |
| CDi | = | Induced Drag Coefficient |
| CD | = | Total Drag Coefficient |
| e | = | Spanwise Efficiency Factor |
| CL | = | Lift Coefficient |
| AR | = | Wing Aspect Ratio |
| Pi | $=$ | 3.14159 |
| CD | $=$ | CDo + CDi |
| CDi | $=$ | (CL x CL) / (Pi x AR $\times$ e) |

Initially a set of drag coefficients was obtained using one of the routines provided in the "BASIC Aircraft Performance" suite. Prior use of this program had indicated it provided only a very approximately correct value, and then only at lower speeds. Using this as a starting point these drag data were revised using an iterative procedure. The drag values would be used to generate a flight envelope, then this envelope would be compared with the quoted aircraft performance (stall speed, maximum speed at low level, maximum speed at altitude and service ceiling). The drag data would then be adjusted as required to better match the known performance of the aircraft.

Table 1 shows the geometric data input into the analysis program, and used to obtain the initial drag estimate for the aircraft. Table 2 shows the final drag data obtained after interation, and used for the final performance assessments. Table 3 shows the typical output for one velocity for the "BASIC Aircraft Performance" drag prediction routine, while Table 4 shows the engine data which was used for this analysis.

Figure 1 shows the estimated variation of the aircraft profile drag coefficient with speed, while Figure 2 shows the corresponding wing spanwise efficiency factor and its variation with speed.

| Table 1 | FILE: (F)VIGGN |  |
| :---: | :---: | :---: |
|  | IDENTIFIER: SAAB JA-3 | 7 VIGGEN |
|  |  | = = = = = = = = = |
|  | ZERO FUEL WEIGHT = <br> FUEL WEIGHT = | 27」20 9790 |
|  | NUMBER OF ENGINES = | 1 |
|  | THRUST MULTIPLIER = | 1 |
|  | FUEL FLOW MULTIPLIER = | 1 |
|  | $C L(M A X)=$ | 1. 25 |
|  | WING===========================0=100 | = = = = = = = = = |
|  | THEORETICAL AREA $=$ | 495.16 |
|  | ASPECT RATIO = | 2.45 |
|  | TAPER RATIO = | 0.07 |
|  | SWEEP OF $\mathrm{X} / \mathrm{C}=$ | 42.0 |
|  | $x / C=$ | 0.25 |
|  | (T/C)MAX $=$ | 0.04 |
|  | X/C LOC OF (T/C)MAX = | $0.4$ |
|  | AIRFOIL RN/C = | 1. $76304 \mathrm{E}-83$ |
|  | HORIZONTAL TAIL===FLAPPED===========: EXPOSED AREA = | $\begin{aligned} & ========== \\ & \text { ?D. } \end{aligned}$ |
|  | EXPOSED ASPECT RATIO $=$ | 0.8 |
|  | EXPOSED TAPER RATIO = | 0.2 |
|  | SWEEP OF $\mathrm{X} / \mathrm{C}$ | 50.0 |
|  | $\mathrm{x} / \mathrm{C}=$ | 0.25 |
|  | ( $T / C) M A X=$ | 0.06 |
|  | $X / C$ LOC OF (T/C)MAX $=$ | 0.4 |
|  | VERTICAL TAIL===SINGLE/FLAPPED====== <br> SINGLE FIN AREA = | $\begin{aligned} & =========== \\ & \text { b } \end{aligned}$ |
|  | GEOMETRIC ASPECT RATIO = | 1.20 |
|  | EXPOSED TAPER RATIO = | 0.12 |
|  | SWEEP OF $\mathrm{X} / \mathrm{C}=$ | 43.0 |



| Table 2 | FILE : | DG)VIGGN |
| :---: | :---: | :---: |
|  | IDENTIFIER : | SAAB JA-3? VIGGEN |
|  | ********** REVIEW DRAG | TABLE ********** |
|  | $\begin{gathered} \text { MACH NO. } \\ 0.400 \end{gathered}$ | $\begin{gathered} \text { CDO } \\ 0.01770 \end{gathered}$ |
|  | 0.600 | -.01730 |
|  | 0.800 | -. 0 |
|  | 0.900 | 0.02150 |
|  | 0.950 | 0.03140 |
|  | 1.000 | 0.04130 |
|  | 1.050 | 0.04420 |
|  | 1.100 | 0.04500 |
|  | 1.200 | 0.04450 |
|  | 1.400 | 0.04290 |
|  | 1.600 | 0.04290 |
|  | 1.800 | 0.04290 |
|  | 2.000 | 0.04290 |
|  | 2.200 | 0.04290 |



| Table 3 |  |  | REFE | FILE: DG <br> SAAB JA- <br> SONIC ZER $M=\square$ $\text { ALT }=$ <br> RN/FT = <br> RENCE WING | ) TEST <br> 37 VIGGE <br> O-LIFT . 600 <br> - <br> $4.2 \mathrm{bE}+$ AREA $=$ <br> AREA | drag <br> 495.2 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | component | SuET | LENGTH | RN | $\begin{aligned} & \text { FORM } \\ & \text { FACTOR } \end{aligned}$ | CF | INTERF FACTOR | CDW | CDO | F |
|  | WING HORIZONTAL | 609.2 143.2 | 13.91 10.74 | 5.93E+0? $4.58 \mathrm{E}+07$ | 1.048 1.073 | $0.0021 ?$ 0.00225 | 1.143 1.351 | 0.00000 0.00000 | 0.00319 0.00094 | 1.580 0.467 |
|  | vertical | 140.0 | 9.12 | $3.89 E+07$ | 1.060 | 0.00231 | 1.340 | 0.00000 | 0.00093 | 0.459 |
|  | fuselage | 880.0 | 50.00 | 2.13E+ロ8 | 1.227 | 0.00181 | 1.015 | 0.00000 | 0.00400 | 1.980 |
|  | misc. | 0.0 | 0.00 | 0.00E+00 | 0.000 | 0.00000 | 0.000 | 0.00000 | 0.0086 | 4.290 |
|  | total | ¢,772.3 |  |  |  |  |  |  | 0.01772 | 8.776 |
|  | CFE $=0.00495$ |  |  |  |  |  |  |  |  |  |

SPAN EFFICIENCY FACTOR $=0.915$


Mach Number
Figure 1



| 0.800 | $\begin{array}{r} 23740 \\ 9,120 \\ 5,120 \end{array}$ | $\begin{array}{r} 59,825 \\ 5 \_837 \\ 3 ヶ 123 \end{array}$ |
| :---: | :---: | :---: |
| 0.900 | $\begin{array}{r} 257187 \\ 9,224 \\ 4,989 \end{array}$ | $\begin{array}{r} 63,471 \\ 5,703 \\ 3,043 \end{array}$ |
| 1.000 | $\begin{array}{r} 26,582 \\ 9,080 \\ 4,281 \end{array}$ |  |
| 1.200 | $\begin{array}{r} 287190 \\ 7,243 \\ 458 \end{array}$ | $\begin{array}{r} 71039 \\ 4 \text { י } 43 \\ 279 \end{array}$ |
| 1.600 |  |  |
| MACH | ALTITUDE ： THRUST | Fロad FEET FUEL FLOW |
| 0.400 |  | $\begin{array}{r} 35,547 \\ 3 \_784 \\ 2,086 \end{array}$ |
| 0.600 |  | $\begin{array}{r} 39 っ 352 \\ 3 \_851 \\ 2 ヶ 125 \end{array}$ |
| 0.800 | $\begin{array}{r} 18,050 \\ 6,503 \\ 3,715 \end{array}$ | $\begin{array}{r} 45,486 \\ 4 っ 162 \\ 2 っ 266 \end{array}$ |
| 0.900 | $\begin{array}{r} 19,36 ? \\ 6 ヶ 861 \\ 3,773 \end{array}$ | $\begin{array}{r} 48,805 \\ 4,391 \\ 2,302 \end{array}$ |
| 1.000 | $\begin{array}{r} 20768 \\ 6,766 \\ 3,479 \end{array}$ | $\begin{array}{r} 51,933 \\ 4,458 \\ 2 ヶ 122 \end{array}$ |
| 1.200 |  | $\begin{array}{r} 60,308 \\ 4,052 \\ 1,053 \end{array}$ |




|  | $\square$ | $\square$ |
| :---: | :---: | :---: |
| 1．200 | $\begin{array}{r} 4,495 \\ 0 \end{array}$ |  |
| 1.400 | $\begin{array}{r} 4.818 \\ \square \end{array}$ |  |
| 1．600 | $\begin{array}{r} 500 \\ \square \end{array}$ | $\begin{array}{r} 13 \\ 0 \end{array}$ |
| 2.800 | $\begin{array}{r} 7,468 \\ 0 \end{array}$ |  |
| 2.200 | $\begin{array}{r} 8.820 \\ 0 \end{array}$ | $\begin{array}{r} \text { b } 2 ⿰ 冫 ⿰ 亻 ⿱ 丶 ⿻ 工 二 十 \end{array}$ |

## PERFORMANCE ESTIMATE

Once a specific set of drag and thrust data has been defined，for a particular aircraft geometric configuration，it is possible to determine the aircraft＇s performance．The most useful initial performance data is the aircraft flight envelope．For the Viggen．this has been estimated for a number of load factors．Table 5 shows the flight envelope data generated by the performance analysis program，while Figure 3 presents the flight envelope in a graphical form．The flight envelope approximates to the published performance values for the aircraft in terms of maximum speeds，stall speed and expected service ceiling．


| LOAD FACTOR＝1 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ＜－－－－－MINIMUM－－－－－＞＜－－－－－MAXIMUM |  |  |  |  |  |
| ALTITUDE | M | KTAS | KEAS | M | KTAS | KEAS |
| 0 | 0．18？ | 124 | 124 | 1．136 | 752 | 752 |
| 5000 | 0.205 | 133 | 124 | 1．123 | 730 | 678 |
| 10．000 | 0．225 | 144 | 124 | 1.091 | เา | 597 |
| 159000 | 0．249 | 156 | 124 | 1．173 | 735 | 583 |
| 20，000 | 0.275 | 169 | 124 | 1.485 | 912 | bь？ |
| 25，000 | 0.306 | 184 | 124 | 1．635 | 984 | bடロ |
| 30，000 | 0.342 | 202 | 124 | 1.762 | \％1039 | 637 |
| 359000 | 0．396 | 228 | 」27 | 1.919 | \％1．06 | 618 |
| 40，000 | 0.494 | 283 | 141 | 2.897 | \％．1204 | 597 |
| 45ヶ000 | 0.597 | 344 | 152 | 1.98 | \％1136 | 502 |
| 50.000 | －．729 | 418 | 164 | 1.818 | 584 | 2วๆ |
| 51,000 | 0.753 | 432 | 165 | 0.977 | 572 | 219 |
| 52．000 | 0．738 | 446 | 16？ | 0.983 | 564 | 211 |
| 53.000 | 0.807 | 463 | 169 | 0．769 | 55b | 203 |
| 54 ¢ 000 | 0.844 | 484 | 172 | 0.751 | 545 | 194 |
| 55，000 | 0.888 | 509 | 177 | 0.915 | 525 | 183 |
| LOAD FACTOR＝ 2 |  |  |  |  |  |  |
|  | ＜－－－－MINIMUM－－－－－＞＜－－－－－MAXIMUM－－－－－－＞ |  |  |  |  |  |
| ALTITUDE | M | KTAS | KEAS | M | KTAS | KEAS |
| 0 | 0.264 | 175 | 175 | 1．131 | 748 | 748 |
| 5，000 | 0．290 | 188 | 175 | 1.113 | 724 | 672 |
| 10.000 | 0.318 | 203 | 175 | 1．068 | 682 | 58b |
| 15ヶ000 | 0．351 | 220 | 175 | 1．123 | 203 | 558 |
| 20，000 | 0.397 | 244 | 178 | 1.3114 | 805 | 589 |
| 25，000 | 0.484 | 291 | 195 | 1.504 | 906 | 607 |
| 30.000 | 0.584 | 344 | 21］ | 1.594 | 939 | 576 |
| 35，000 | 0．726 | 419 | 234 | 1.003 | 578 | 323 |
| 40，000 | 0．000 | $\square$ | $\square$ | －．000 | $\square$ | $\square$ |


| LOAD FACTOR = 3 |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | <----MINIMUM-----> <-----MAXIMUM-----> |  |  |  |  |  |
| ALTITUDE | M | KTAS | KEAS | M | KTAS | KEAS |
| $\square$ | 0.324 | 214 | 214 | 1.123 | 743 | 743 |
| 5,000 | 0.356 | 232 | 215 | 1.058 | 688 | 639 |
| 10.000 | 0.415 | 2 b | 228 | 1.036 | b6l | 5b8 |
| 159000 | 0.492 | 309 | 245 | 1.049 | 657 | 522 |
| 20.000 | 0.588 | 361 | 264 | 1.051 | 646 | 472 |
| 25,000 | 0.700 | 422 | 283 | 1.006 | 60 | 406 |
| 30,000 | 0.845 | 498 | 305 | 0.752 | 56 | 344 |
| 35,000 | 0.000 | $\square$ | $\square$ | 0.000 | $\square$ | $\square$ |
| LOAD FACTOR = 4 |  |  |  |  |  |  |
|  | <-----MINIMUM-----> |  |  | <-----MAXIMUM-----> |  |  |
| ALTITUDE | M | KTAS | KEAS | M | KTAS | KEAS |
| $\square$ | 0.413 | 273 | 273 | 0.989 | 654 | 654 |
| 5000 | 0.476 | 309 | 287 | 1.000 | b50 | 603 |
| 10.000 | 0.554 | 354 | 304 | 1.000 | b38 | 549 |
| 15,000 | 0.653 | 409 | 325 | 0.770 | 620 | 492 |
| 20.000 | 0.765 | 470 | 343 | 0.768 | 594 | 434 |
| 25,000 | 0.000 | $\square$ | $\square$ | 0.000 | $\square$ | $\square$ |
| LOAD | FACTOR | $=5$ |  |  |  |  |
|  | <----MINIMUM-----> |  |  | <-----MAXIMUM-----> |  |  |
| ALTITUDE | M | KTAS | KEAS | M | KTAS | KEAS |
| $\square$ | 0.517 | 342 | 342 | 0.000 | $\square$ | $\square$ |
| 5000 | 0.598 | 389 | 361 | 0.976 | 635 | 589 |
| 1000000 | 0.692 | 442 | 380 | 0.768 | 618 | 531 |
| 159000 | 0.810 | 507 | 403 | 0.939 | 589 | 46 ? |
| 20,000 | 0.000 | $\square$ | $\square$ | 0.000 | $\square$ | $\square$ |



Mach Number
Figure 3

| LOAD FACTOR = b |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\begin{gathered} <---- \text { MINIMUM-----> } \\ \text { M KTAS KEAS } \end{gathered}$ |  |  | <-----MAXIMUM-----> |  |  |
| ALTITUDE |  |  |  | M | KTAS | KEAS |
| $\square$ | 0.b2b | 414 | 414 | 0.000 | $\square$ | $\square$ |
| 5,000 | 0.72l | 469 | 435 | 0.749 | 617 | 573 |
| 10.000 | 0.846 | 540 | 464 | 0.917 | 58 | 503 |
| 1,59000 | 0.000 | $\square$ | $\square$ | 0.000 | $\square$ | $\square$ |
| LOAD | FACTOR $=$ ? |  |  |  |  |  |
|  | <----MINIMUM-----> |  |  | <-----MAXIMUM-----> |  |  |
| ALTITUDE | M | KTAS | KEAS | M | KTAS | KEAS |
| 0 | 0.744 | 492 | 492 | 0.933 | bl? | 617 |
| 000 5 | 0.898 | 584 | 542 | 0.902 | 58 | 545 |
| 10.000 | 0.000 | $\square$ | $\square$ | 0.000 | $\square$ | $\square$ |

In an attempt to verify the performance data estimated here with the published performance figures a ferry mission was defined. Table 6 shows the specific legs making up this ferry mission, while Figure 4 displays the results obtained from the analysis program. The published figures indicate a ferry range for the aircraft of 1250 miles (2000 kilometres). The computer prediction gives calculated a ferry range of 1088 miles (945 nautical miles).



Figure 4

Further checking of the drag data estimated here was carried out by comparing a climb to altitude．This information was provided in the published data for the aircraft，with a climb to 32，810 feet（10，000 metres）quoted as taking 1.4 minutes（84 seconds），for an aircraft loaded with four AAM stores plus $50 \%$ internal fuel，and climb performed at maximum afterburner．The analysis program indicated a time to 32,000 feet，for the same aircraft configuration，would take 1.7 minutes（102 seconds）． The program output for this climb is presented in Table 7，with Figure 5 showing the actual，and estimated，time to climb in a graphical format．

## Table 7

> | CLIMB VERIFICATION |  |
| :--- | :--- |
| FILE | $:$ |
|  | CF)VIGGN |
| AIRCRAFT | $:$ SAAB JA-37 VIGGEN |
| ENGINE | $:$ VOLVO FLYGMOTOR RM-AB TURBOFAN |
| MISSION | $:$ |
| SLIMB TO 32810 FEET |  |
| AR | 495.16 |
| NO OF ENGINES: | 1 |

| TIME MIN | $\begin{array}{r} \text { ALT } \\ \text { FT } \end{array}$ | $\begin{gathered} \text { RANGE } \\ \text { NM } \end{gathered}$ |  | $\begin{aligned} & \text { WEIGHT } \\ & \text { LBS } \end{aligned}$ | FUEL LBS | $\begin{aligned} & \text { TAS } \\ & \text { KTS } \end{aligned}$ | $\begin{aligned} & \text { EAS } \\ & \text { KTS } \end{aligned}$ | MACH | $\begin{aligned} & R / C \\ & F T / M I N \end{aligned}$ | $\begin{aligned} & \text { SR } \\ & \text { NM/LB } \end{aligned}$ | CL | CDD | $\begin{aligned} & \text { FUEL } \\ & \text { FLOW } \\ & \text { LB/HR } \end{aligned}$ | THRUST | E | L／D |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.0 |  | $\square$ | $\square$ | 0\％ 3 | ๆ，ア90 | $\square . \square$ | $\square . \square$ | 0.000 | $\square$ | 0．0000 | 0.000 | －． | $\square$ | $\square$ | 0．000 | 0.0 |
| CLIMB TO | 32810 F | FEET AT | BES | T R／C |  |  |  |  |  |  |  |  |  |  |  |  |
| $0 . \square$ |  | $\square$ | $\square$ | 067910 | ๆ，ア90 | 555.4 | 555.4 | 0.840 | 29，ヨ27 | 0.0074 | － | － | 747654 | 29ッ625 | 0.764 | 3.6 |
| 0．1 | 2ヶ000 |  | 1 | 36ヶ82b | ワっ706 | 551．3 | 535.4 | 0.837 | 28っbا | 0．0076 | －．077 | 0．01919 | 727181 | 28ヶ644 | 0．764 | 3.8 |
| 0．1 | 47000 |  | 1 | 36ヶ742 | 9ヶเว2 | 551．0 | 519．3 | 0.845 | 27ヶ906 | －．0079 | 0．081 | 0.01940 | レ9ヶ82b | 27，654 | 0．764 | 4.0 |
| 0.2 | b．000 |  | 2 | 36ヶ69 | 9，539 | 551．5 | 504.4 | 0．851 | 27， | 0.0082 | 0.086 | 0.0196 | 67ヶ371 |  | 0.764 | 4.1 |
| 0.3 | B |  | 3 | 36，576 | 9，456 | 552.5 | 490.0 | 0.859 | 26っ182 | 0.0085 | 0．091 | －．01975 | 64ヶ872 | 1 25174 | 0.764 | 4.3 |
| 0.4 | 10．000 |  | 3 | 36，473 | 9， 373 | 553．7 | 476．1 | 0．8b？ | 25っ23l | 0.0089 | －．096 | － 0.020 | b2っ284 | 64．71 | 0.764 | 4.4 |
| 0.4 | 12ヶ000 |  | 4 | 36，411 | ワっ291 | 555.5 | 462．8 | 0.877 | 24.146 | 0.0093 | －．101 | －．02062 | 59っ696 | 23－6ا | 0.764 | 4.5 |
| 0.5 | 14.800 |  | 5 | 3ьヶэコๆ | ๆ， 209 | 541．5 | 436.7 | 0．8bl | 22ヶ869 | 0.0096 | 0．114 | －．02002 | 56，196 | 2ᄅっ260 | 0.764 | 5．1 |
| 0.6 | 16．000 |  | 6 | 36，24？ | ワっ12？ | 537．1 | 419.5 | －．8bl | 21， | －．0101 | －．123 | 0.02001 | 53っ25？ | 2lı097 | 0．764 | 5.4 |
| 0.7 | 18．000 |  | ？ | 36ヶリ65 | 9，045 | 53b．8 | 405.7 | 0．8b？ | 20，524 | 0.0106 | －．131 | 0.02025 | 50，574 | 20．046 | 0.764 | 5.7 |
| 0.8 | 20．000 |  | 7 | 36，082 | ロッフレ2 | 538．］ | 393．3 | 0．87b | 19，417 | －0．0112 | 0．139 | 0.02058 | 48－005 | 19．050 | 0.764 | 5.8 |
| 0.7 | 22ヶ000 |  | 8 | 35ヶワワワ | 8 ロロ79 | 538．6 | 380.5 | 0.884 | 18っ105 | 0.0119 | 0．148 | －．02088 | 45722l | 17ヶワ27 | 0.764 | b． 0 |
| 1.0 | 24.800 |  | q | 655971 | 8， | 528．b | 36ロ．8 | 0.875 | 16，bl5 | 0．0126 | 0．165 | 0.02053 | 41，¢7？ | 16ヶ63 | 0.764 | b． 5 |
| 1.2 | 2bı000 |  | 11 | 35ヶ831 | 8， | 525.0 | 345．7 | 0．87b | 157295 | 0.0134 | －．179 | －．02058 | 39，178 | 15，524 | 0．764 | ¢． 9 |
| 1.3 | 28ヶ000 |  | 12 | 35，745 | 8， 225 | 525．8 | 334.2 | 0.884 | 14っ120 | 0.0143 | －1．191 | 0.02091 | 36，71？ | 14，55b | 0．764 | 7.0 |
| 1.4 | 30.000 |  | 13 | 35467 | 8 B 537 | 524．8 | 321．7 | 0．891 | 12，945 | 0.0153 | 0.205 | －02114 | 34， | 13，597 | 0．764 | 7.3 |
| 1.6 | 32ヶ000 |  | 14 | 35，5b | 8.446 | 514.4 | 303．7 | 0.881 | 117104 | 0.0168 | 0.230 | 0．02076 | 30ヶ600 | 12．185 | 0.764 | 7.7 |
| 1.7 | 32，810 |  | 15 | 35，529 | 8.409 | 513.0 | 298．5 | 0．881 | 10，4b2 | －．0175 | ロ．2зв | －．02079 | 29，332 | 11.697 | 0．764 | 7.8 |



Figure 5


Figure 6

As there was a discrepancy with the actual and calculated ferry ranges (1250 miles compared with 1088 miles), a little further investigation was carried out. The actual ferry range was at an unspecified cruising altitude, so the ferry mission was run for a range of different cuise altitudes. The results of this analysis are shown in Figure 6 . This indicated a maximum achievable range of about 960 nautical miles ( 1105 miles), which is about $13 \%$ less than the published figure for tha actual aircraft.

Overall, the discrepancies in the ferry range and climb performance are most likely due to the use of less than perfect engine performance data. Better engine data would probably give a closer match to the actual aircraft performance. At present, the engine and drag data currently used in the computer analysis program will give conservative performance results.

Finally, a table of data has been provided to define the predicted manoeuvre performance of the aircraft. This data is for a range of velocities and altitudes, and is presented in Table 8. Estimates are given for maximum turnrate, specific excess power, specific range and a few other parameters.


| ALTITUDE $=1.0000$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ＜－－－－－－－－－－－－－MAX POWER－－－－－－－－－－－－－－＞＜－－－－－－－CRUISE POWER－－－－－－－－－＞ |  |  |  |  |  |  |  |  |  |
|  |  |  | T RATE | TR／FF | P－SUB－S | S RNG | F FLOw | THRUST |  |
| MACH | CL－M | N－MAX | DEG／S | DEG／LG | FT／SEC | NM／LB | LB／HR | LB／ENG | CL－C |
| 0.30 | 1． 250 | 1．77 | 8.4 | 0.6 | 140．7 | 0.0685 | 2ヶフ72 | 47640 | 0．704＊ |
| 0.40 | 1． 145 | 2．89 | 1.1 .6 | 0.7 | 213.3 | 0．1231 | 2ヶ074 | 3，587 | 0．396 |
| 0.50 | 0．917 | 3.62 | 1.1 ． 9 | 0.8 | 280.4 | 0．1．524 | 27094 | 37615 | 0.254 |
| 0.60 | －．7bl | 4.32 | $12 . \square$ | 0.8 | 342.2 | 0.1545 | 2，478 | 4 Tl 7 | －．176 |
| 0.70 | 0．655 | 5.06 | 1．2．1 | 0.8 | 408．6 | 0.1442 | $3 ヶ 098$ | 57084 | －．129 |
| 0.80 | 0.573 | 5.78 | 12．2 | 0.7 | 470.6 | 0.1311 | 3 3896 | 6っ2bロ | 0．097 |
| 0.90 | 0.485 | b．20 | 1．6．6 | 0.7 | 483.6 | 0.0974 | 5 | ๆって2l | 0.078 |
| 1.00 | 0.246 | 3.88 | 6.4 | 0.3 | 179．7 | 0.0132 | 48 ¢297 | 21，235 | 0.063 |
| 1.10 | 0.000 | 1.00 | 0.0 | 0.0 | －17．6 | 0.0097 | 70，729 | 27っ862 | 0.052 |
| ALTITUDE $=20000$ |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| MACH | CL－M | N－MAX | T RATE DEG／S | TR／FF DEG／LG | $P-S U B-S$ <br> FT／SEC | $S$ RNG NM／LB | $\begin{aligned} & \text { F FLOW } \\ & \text { LB/HR } \end{aligned}$ | THRUST <br> LB／ENG | CL－C |
| 0.30 | 1．250 | 1．19 | 3.8 | 0.4 | 68．8 | 0.0344 | 57355 | Ьっ269 | 1．053＊ |
| 0.40 | 1．176 | 2.02 | 7.8 | 0.8 | 128．6 | 0.0944 | 27604 | 4 T 181 | 0.592 |
| 0.50 | 0.764 | 2.55 | в． 3 | 0.8 | 183．0 | 0.1410 | 2ヶ】78 | 3，558 | 0.379 |
| 0.60 | 0.807 | 3.07 | 8.6 | 0.8 | 233．8 | 0.1680 | 2，195 | 3ヶ586 | －．263 |
| 0.70 | 0.703 | 3.63 | 8.9 | 0.8 | 291．3 | 0.1750 | 2，45？ | 37984 | －．193 |
| 0.80 | －．b22 | 4.20 | ๆ．］ | 0.7 | 347.6 | 0.1700 | 2ヶ891 | 4 ¢ 634 | 0.148 |
| 0.90 | 0.538 | 4.60 | 8． 9 | 0.7 | 374.4 | －．1329 | $4 ヶ 762$ | 6，522 | 0．1．7 |
| 1.00 | 0.324 | 3.42 | 5.8 | 0.4 | 197.0 | 0.0200 | 30，761 | 14，524 | 0.095 |
| 1.10 | 0.208 | 2．ь6 | 4.0 | 0.3 | 118．4 | 0.0147 | 45っ263 | 18，947 | 0.078 |
| 1.20 | 0．138 | 2.09 | 2.7 | 0.2 | 68．ᄅ | 0.0135 | 54ヶロワ | 22ヶ」ア6 | 0．06 |
| 1.30 | 0.113 | 2.02 | 2.4 | 0.1 | bl．b | 0.0123 | 64，947 | 25，436 | 0.056 |
| 1.40 | 0.087 | 1.80 | 1.9 | 0．1 | 45.6 | 0.0115 | 74795？ | 28ヶ863 | 0.048 |
| 1.50 | 0．031 | 1.00 | 0.0 | 0.0 | －9．5 | 0.0107 | 86， 317 | 33ヶ033 | 0.042 |


| ALTITUDE $=3000$ |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |
| MACH | CL－M | N－MAX | $\begin{aligned} & \text { T RATE } \\ & \text { DEG/S } \end{aligned}$ | $\begin{aligned} & \text { TR/FF } \\ & \text { DEG/LG } \end{aligned}$ | $\begin{aligned} & P-S U B-S \\ & F T / S E C \end{aligned}$ | $\begin{aligned} & S \text { RNG } \\ & N M / L B \end{aligned}$ | $\begin{aligned} & \text { F FLOW } \\ & \text { LB/HR } \end{aligned}$ | $\begin{aligned} & \text { THRUST } \\ & \text { LB/ENG } \end{aligned}$ | CL－C |
|  |  |  |  |  |  |  |  |  |  |
| 0.40 | 1．189 | 1.30 | 3.9 | 0.6 | 42．8 | －ロご1 | ワา040 | 5759 | －．715＊ |
| 0． 50 | －．981 | 1.68 | 5.0 | 0． 7 | 89．5 | 0．0945 | 3ヶ118 | 47155 | －．585＊ |
| 0.60 | ロ．838 | 2.06 | 5.6 | 0．7 | 134.0 | 0．1547 | 2ヶ285 | 3ヶ607 | 0.406 |
| 0．70 | －．732 | 2.45 | 5.7 | －． 7 | 177．2 | 0．1854 | 2ヶ225 | 3 ヶ523 | －．2ワワ |
| 0.80 | 0.650 | 2．84 | b．2 | 0.7 | 219．4 | －．2001 | 2ヶ356 | $3 ヶ 723$ | ロ．2こワ |
| 0.70 | 0．573 | 3．17 | b． 2 | 0.6 | 249．3 | －1．1526 | 3，475 | 4 ヶ7ワ4 | 0．181 |
| 1.00 | －．378 | 2．58 | 4.4 | 0.4 | 154．3 | －．0284 | 20ヶ786 | ワッチ12 | 0.146 |
| 1.10 | ロ．283 | 2． 34 | 3.6 | 0.3 | 128．？ | －－－2 | こワっここ5 | 12， 756 | －．121 |
| 1．20 | ロ．231 | 2．27 | 3．1 | ロ．2 | 1224．4 | －．0203 | 347858 | 14ヶ824 | 0．102 |
| 1.30 | －．203 | 2．34 | 3.0 | ロ．2 | 133．9 | －．0183 | 417791 | 16ヶタワ7 | 0.087 |
| 1.40 | －．177 | 2． 37 | 2．8 | ロ．2 | 138.0 | 0．0170 | 48，562 | 19ヶロ88 | 0.075 |
| 1.50 | －．146 | 2．24 | 2.5 | －．1 | 119．0 | －．0157 | 56，170 | 21ヶ756 | 0.065 |
| 1.60 | －．113 | 1．98 | 2．0 | －．1 | 86． 3 | －．0148 | b3ヶ664 | 24ヶ624 | 0.057 |
| 1.70 | 0．077 | 1.52 | 1.3 | －．1 | 38．5 | 0．0141 | 70ヶ942 | こアッ68ロ | 0.051 |
| 1.80 | 0．013 | 1.00 | 0.0 | 0.0 | －26．5 | 0．0136 | 77，950 | 30ヶ932 | 0.045 |
| ALTITUDE $=40000$ |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| MACH |  |  |  |  |  |  |  |  |  |
| MACH |  |  |  |  |  |  |  |  |  |
| 0.50 | －．950 | 1．01 | 0.6 | －．2 | 2．11 | 0.0204 | 14， 4 － | 57705 | ロ．937＊ |
| 0.60 | －．813 | 1．25 | 2.4 | 0.5 | 36.1 | 0.0413 | 8 ¢ 333 | 47413 | －．651＊ |
| 0．70 | －．712 | 1.49 | 3.0 | 0.6 | 67.2 | 0.0754 | 5 ¢ 3 ¢ | 3ヶ788 | 0.478 |
| 0．80 | 0.634 | 1． 73 | 3.4 | 0.6 | 96． 3 | －．1198 | 3ヶタコワ | 37541 | 0．366 |
| 0.70 | 0． 553 | 1.91 | 3.4 | 0．6 | 1113.7 | －．1033 | 4ヶ798 | 37955 | 0．289 |
| 1.00 | －．360 | 1． 54 | 2．2 | 0.4 | 57．6 | 0．0362 | 15485 | 7，048 | 0．234 |
| 1.10 | －．292 | 1．51 | 2．0 | 0.3 | 56．9 | －．0301 | 20ヶ985 | ロッフワ2 | －．194 |
| 1．20 | －．260 | 1.60 | 2．0 | ロ．2 | 72.9 | －．028？ | 23ヶ974 | 107846 | 0．163 |
| 1.30 | 0．241 | 1.74 | 2．1 | ロ．2 | 93．7 | －．026？ | 27ヶ964 | 11ヶ2ア？ | 0.139 |



